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## Turbulent diffusivities derived from simulations

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**Abstract.** By employing direct simulations of turbulent magneto-convection we determine the turbulent diffusivities, such as the turbulent magnetic diffusivity, the eddy viscosity and the turbulent heat conductivity. The fluid extends over one scale height and is confined between impenetrable boundaries. With our technique it is essential for the determination of such quantities to enforce a non-vanishing mean current and a gradient in the mean velocity. We find that the order of magnitude obtained for the various turbulent diffusivities is in some cases compatible with the customary expression  $\frac{1}{3}u_t\ell$ , where  $u_t$  is the rms-velocity and  $\ell = d$  is the mixing length which is here taken to be the depth of the layer. However, there is evidence that the eddy viscosity does not allow a suitable description in the present cases where the turbulence is caused by convection. Finally, results for the mean Lorentz force are presented and discussed in the context of recent predictions based on the first order smoothing approach.

**Key words:** stellar convection - turbulence - turbulent diffusion - mean-field dynamo - the Sun: magnetic fields

### 1. Introduction

In a previous paper (Brandenburg et al., 1990, hereafter referred to as Paper I) we have described a method for determining mean-field transport coefficients, such as the  $\alpha$ -effect and the turbulent magnetic diffusivity, by means of direct simulations of turbulent magneto-convection. These turbulent transport coefficients describe the dependence of certain correlation functions on the mean magnetic field  $\langle \mathbf{B} \rangle$ , the mean velocity  $\langle \mathbf{u} \rangle$ , and other quantities. They allow closure of the differential equations for  $\langle \mathbf{u} \rangle$ ,  $\langle \mathbf{B} \rangle$ , and other (thermodynamic) quantities. Such equations are employed for example in mean-field dynamo theory (e.g. Krause & Rädler, 1980).

In Paper I we chose boundary and initial conditions such that a systematic average magnetic field with a certain orientation is present. By "systematic" we mean a mean field whose properties are independent of details of the initial conditions, so that its spatial variation and magnitude are then more-or-less predictable. This approach reflects the intention of simulating the turbulent flow only in a small *test volume* in the solar convection zone.

Our previous results have indicated the importance of anisotropies in the  $\alpha$ -effect. The determination of the turbulent magnetic diffusivity  $\eta_t$ , however, seemed somewhat unreliable because negative values were typically obtained. This is unphysical, because the mean-field equations possess stable solutions only for positive turbulent diffusivities.

One of the aims of this paper is to reconsider the determination of  $\eta_t$ . In the theory of mean-field electrodynamics it is shown that the turbulent electromotive force  $\langle \mathbf{u}' \times \mathbf{B}' \rangle$  can be expressed as a linear functional of  $\langle \mathbf{B} \rangle$ . For example in the simplest case of isotropic turbulence one finds

$$\langle \mathbf{u}' \times \mathbf{B}' \rangle = \alpha \langle \mathbf{B} \rangle - \eta_t \text{curl} \langle \mathbf{B} \rangle$$

(e.g. Roberts & Sowards, 1975). In the models investigated in Paper I the  $x$ - and  $y$ -components were equally preferred. Typically, the horizontal components of  $\text{curl} \langle \mathbf{B} \rangle$  are then nearly vanishing and the vertical component of  $\text{curl} \langle \mathbf{B} \rangle$  vanishes identically since  $\text{div} \langle \mathbf{B} \rangle = 0$  and by definition of the averages adopted (cf. Paper I). Thus,  $\eta_t$  multiplies a very small quantity. This makes a reliable determination of  $\eta_t$  impossible. It appears therefore necessary to impose a systematic (vertical) gradient in  $\langle \mathbf{B} \rangle$ . This can be done by choosing appropriate boundary conditions. The same concept can be applied to the determination of  $\nu_t$  by imposing a systematic vertical gradient in the average velocity  $\langle \mathbf{u} \rangle$ .

This paper is organized as follows. In Sect. 2 we summarize the basic equations and describe briefly the model for simulating magneto-convection. The equations for determining  $\alpha$  and  $\eta_t$  are given in Sect. 3. Results for  $\eta_t$  and also for the eddy viscosity and the turbulent heat conductivity are shown in Sect. 4. Finally, we discuss implications for the mean Lorentz force (Sect. 5) and give our conclusions (Sect. 6).

## 2. Simulating magneto-convection

We consider a fully compressible fluid heated from below and take the dynamical effects of magnetic fields and rotation into account. We are interested in the lower layers of the convection zone and can treat radiation therefore in the diffusion approximation. We assume all variables to be periodic in the horizontal direction. This is numerically convenient and avoids artificial boundaries. (However, it is then impossible to include the centrifugal force in the momentum equation; see discussion in Paper I.)

We solve the equations for conservation of mass, momentum, energy, and the induction equation in the form

$$\frac{D \ln \rho}{Dt} + \operatorname{div} \mathbf{u} = 0, \quad (1)$$

$$\frac{D \mathbf{u}}{Dt} = -\frac{p}{\rho} \nabla \ln p + \mathbf{g} - 2\boldsymbol{\Omega} \times \mathbf{u} + \frac{1}{\rho} \mathbf{J} \times \mathbf{B} + \frac{\mu}{\rho} (\nabla^2 \mathbf{u} + \frac{1}{3} \nabla \nabla \cdot \mathbf{u}), \quad (2)$$

$$\frac{D e}{Dt} = -\frac{p}{\rho} \operatorname{div} \mathbf{u} + \frac{\mathcal{K}}{\rho} \nabla^2 e + Q_{\text{visc}} + Q_{\text{Joule}}, \quad (3)$$

$$\frac{\partial \mathbf{B}}{\partial t} = \operatorname{curl} (\mathbf{u} \times \mathbf{B} - \mathbf{J} / \sigma), \quad (4)$$

where  $e$  is the specific internal energy of the gas which we assume to be ideal, i.e.  $p/\rho = (\gamma - 1)e$ . Here,  $\gamma$  is the ratio of the specific heats  $c_p$  and  $c_v$ , which are assumed to be constant.  $Q_{\text{visc}}$  is the rate of viscous heating, and  $Q_{\text{Joule}} = \mathbf{J}^2 / \rho \sigma$  is the rate of Joule heating per unit mass,  $\mathbf{J} = \operatorname{curl} \mathbf{B} / \mu_0$  is the electric current, and  $\sigma$  the electric conductivity. If the condition  $\operatorname{div} \mathbf{B} = 0$  is satisfied by the initial field,  $\operatorname{div} \mathbf{B}$  remains zero. In the derivation of Eqs. (2) and (3) we have assumed constant values for  $\mu$  and  $\mathcal{K}$ .

As in Paper I we exclude penetration of the motions through the boundaries of the computational volume. If not stated otherwise we require the horizontal components of viscous and magnetic stress to vanish on both boundaries, i.e.  $u_{1,3} = u_{2,3} = u_3 = 0$  and  $B_1 = B_2 = 0$  at the top and bottom. Commas denote derivatives and index 3 refers to the  $z$ -direction. We keep  $e$  constant at the top and prescribe the vertical gradient of  $e$  on the bottom.

The initial velocity field consists of a superposition of many, spatially smooth, but randomly distributed perturbations in all three components. We take the ratio between horizontal and vertical extent of the model (aspect ratio)  $A = 2$ , a density contrast  $\chi = 2$ , and  $\gamma = 5/3$ . The Chandrasekhar number is  $Q = B_0^2 d^2 / \mu_0 \mu \eta = 72$ , and the Taylor number is  $\text{Ta} = 10^4$ . The two Prandtl numbers,  $\text{Pr}$  and  $\text{P}_m$ , are taken to be unity. Non-dimensional quantities are introduced by measuring time in sound travel times (see Paper I). The unit length is the depth of the layer. Density is measured in units of the initial density at the top,  $\rho_0$ .

We solve the equations (1)-(4) numerically, using a modification of the code by Nordlund and Stein (1989), that employs a second order Adams-Bashforth time advance and spatial derivatives calculated from cubic splines. Further details were described in Paper I. The calculations were carried out on the Cray XMP-EA/432 of the National Computing Center of Finland. For a resolution of  $31^3$  meshpoints the code needs about 0.1-0.2 sec real time per time step and 1.3 Mwords of memory. A typical run covering one diffusion time (500 sound travel times) requires  $10^5$  timesteps.

## 3. Determining transport coefficients from simulations

We split the velocity and the magnetic field into mean and fluctuating parts, i.e.  $\mathbf{u} = \langle \mathbf{u} \rangle + \mathbf{u}'$  and  $\mathbf{B} = \langle \mathbf{B} \rangle + \mathbf{B}'$ . We adopt here a combined horizontal and temporal average, i.e.  $\langle f \rangle = \int dt dx dy f / \int dt dx dy$ . Averaging the induction equation (4) leads to a new term

$$\mathcal{E} = \langle \mathbf{u}' \times \mathbf{B}' \rangle. \quad (5)$$

In the theory of mean-field electrodynamics  $\mathcal{E}$  is expressed as a linear functional of  $\langle \mathbf{B} \rangle$  with

$$\mathcal{E}_i = \alpha_{ij} \langle \mathbf{B}_j \rangle - \beta_{ijk} \partial_k \langle \mathbf{B}_j \rangle. \quad (6)$$

(e.g. Krause & Rädler, 1980). In Paper I we concentrated primarily on the determination of  $\alpha_{ij}$ . The basic result was that only an anisotropic  $\alpha$ -tensor can explain the numerically determined dependence  $\mathcal{E} = \mathcal{E}(\mathbf{B})$ . Writing  $\alpha_{ij} = \alpha_1 \delta_{ij} + \alpha_2 \hat{g}_i \hat{g}_j$  it turned out that  $\alpha_1$  and  $\alpha_1 + \alpha_2$  have opposite signs. Here,  $\hat{g}$  is the unit vector in the direction of gravity.

In the following we wish to determine the  $\beta$ -tensor. The simplest possible form for  $\beta_{ijk}$  is proportional to the totally antisymmetric tensor  $\epsilon_{ijk}$ . Writing  $\beta_{ijk} = \eta_i \epsilon_{ijk}$  we have then

$$\mathcal{E} = \alpha_H \langle \mathbf{B}_H \rangle + \alpha_V \langle \mathbf{B}_V \rangle - \eta_i \mu_0 \langle \mathbf{J} \rangle, \quad (7)$$

where  $\langle \mathbf{B}_H \rangle = \hat{x} \langle B_x \rangle + \hat{y} \langle B_y \rangle$ ,  $\langle \mathbf{B}_V \rangle = \hat{z} \langle B_z \rangle$ , and  $\mu_0 \langle \mathbf{J} \rangle = \operatorname{curl} \langle \mathbf{B} \rangle$ .  $\alpha_H$ ,  $\alpha_V$ , and  $\eta_i$  can be readily determined from this equation by multiplying with  $\langle \mathbf{B}_V \rangle$ ,  $\langle \mathbf{B}_H \rangle$ , and  $\langle \mathbf{J} \rangle$ . Note that  $\langle J_z \rangle = 0$  by definition of the horizontal averages adopted. We then find

$$\alpha_V = \mathcal{E}_z / \langle B_z \rangle, \quad (8)$$

$$\alpha_H = \frac{(\mathcal{E} \cdot \langle \mathbf{B}_H \rangle) \langle \mathbf{J} \rangle^2 - (\mathcal{E} \cdot \langle \mathbf{J} \rangle) (\langle \mathbf{J} \rangle \cdot \langle \mathbf{B}_H \rangle)}{\langle \mathbf{B}_H \rangle^2 \langle \mathbf{J} \rangle^2 - (\langle \mathbf{J} \rangle \cdot \langle \mathbf{B}_H \rangle)^2}, \quad (9)$$

$$\eta_i \mu_0 = -\frac{(\mathcal{E} \cdot \langle \mathbf{J} \rangle) \langle \mathbf{B}_H \rangle^2 - (\mathcal{E} \cdot \langle \mathbf{B}_H \rangle) (\langle \mathbf{J} \rangle \cdot \langle \mathbf{B}_H \rangle)}{\langle \mathbf{B}_H \rangle^2 \langle \mathbf{J} \rangle^2 - (\langle \mathbf{J} \rangle \cdot \langle \mathbf{B}_H \rangle)^2}. \quad (10)$$

Although we have always used the above expressions, it is worthwhile to note for the purpose of discussion that a good approximation is usually  $\alpha_H = \mathcal{E} \cdot \langle \mathbf{B}_H \rangle / \langle \mathbf{B}_H \rangle^2$  and  $\eta_i \mu_0 = -\mathcal{E} \cdot \langle \mathbf{J} \rangle / \langle \mathbf{J} \rangle^2$ .

## 4. Turbulent diffusivities

### 4.1. The turbulent magnetic diffusivity

As discussed in the Introduction we impose here a gradient of the  $y$ -component of  $\langle \mathbf{B} \rangle$  by replacing the boundary condition  $B_2 = 0$  at top and bottom by

$$\begin{aligned} B_2 &= 0 & \text{at the top,} \\ B_2 &= B_0 & \text{at the bottom.} \end{aligned} \quad (11)$$

This leads to a systematic electric current in the  $x$ -direction. The resulting depth dependence of  $\eta_i$  is displayed in the lower panel of Fig. 1. The corresponding profile of  $\alpha_H$ , derived from Eq. (9), is shown in the upper panel. The results for  $\alpha_H$  and  $\eta_i$  are more-or-less independent of the magnetic field strength (cf. dotted and solid lines in Fig. 1). This means that a linear functional dependence  $\mathcal{E} = \mathcal{E}(\mathbf{B})$  is in principle justified. The

resulting turbulent magnetic diffusivity, derived from Eq. (10), has then a *positive* extremum in the middle of the layer with  $\max(\eta_t) \approx 5\eta$ . This value seems to be very small. This is a consequence of the small Reynolds number  $Re = u_t d/\nu$  which is in the present case approximately 25. (Much higher values are normally not accessible with only 31 meshpoints in one direction.) The customary expression for the turbulent diffusivity is  $\frac{1}{3}u_t \ell$ , where  $u_t$  is the rms-velocity. Assuming the mixing length to be the depth of the layer ( $\ell = d$ ) we find here  $\eta_t \approx 0.2u_t \ell$ .

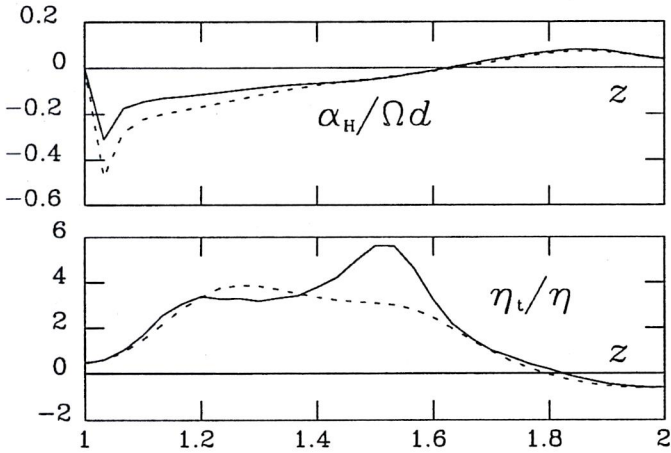


Fig. 1. The profiles of  $\alpha_H$  (normalized with  $\Omega d$ , upper panel) and  $\eta_t$  (normalized with  $\eta$ , lower panel) for  $Q = 72$ . The dotted curves refer to a run with  $Q = 31$

#### 4.2. Eddy viscosity?

It is tempting to determine the eddy viscosity  $\nu_t$  similarly by imposing a systematic gradient in  $\langle \mathbf{u} \rangle$ . The usual Boussinesq ansatz for the Reynolds stress is

$$\langle u'_i u'_j \rangle = -\nu_t (\langle u_{i,j} \rangle + \langle u_{j,i} \rangle) - \mu_t \delta_{ij} \text{div} \langle \mathbf{u} \rangle. \quad (12)$$

Further (non-diffusive) terms enter into Eq. (12) due to the presence of rotation. In the compressible case further terms occur. However, in the cases considered below we find always  $\langle \rho' u'_i \rangle \ll \langle \rho \rangle \langle u_i \rangle$ .

A systematic gradient in the velocity can be achieved by replacing the boundary condition  $u_{2,3} = 0$  by

$$u_{2,3} = U_{23} \quad \text{at top and bottom,} \quad (13)$$

where  $U_{23}$  is some constant. This boundary condition is a generalization of the stress free condition  $u_{2,3} = 0$ , which is in contrast to a rigid one where  $u_2$  is prescribed.

We have computed models for different values of  $U_{23}$ . The resulting profiles of  $\langle u'_2 u'_3 \rangle$  and  $\langle u_{2,3} \rangle$  are shown in Fig. 2. Note that  $\langle u'_2 u'_3 \rangle$  is always negative. This means that vertical transport of momentum  $\rho u_2$  is upwards, i.e. in the negative  $z$ -direction. In the upper parts  $u_2$  is smaller than in the lower parts. Downflow transports a deficit velocity into regions with larger  $u_2$  and vice versa. It is remarkable that the gradient  $\langle u_{2,3} \rangle$ , imposed at both boundaries, becomes very small in the inner parts of the layer. In fact,  $\langle u_{2,3} \rangle$  does even change

sign. This means that in this case the vertical transport of momentum cannot be described by positive eddy viscosity coefficients. In other words, the simple expression (12) is *not* suitable to describe the Reynolds stress  $\langle u'_2 u'_3 \rangle$  by means of gradients of the average velocity  $\langle u_2 \rangle$ .

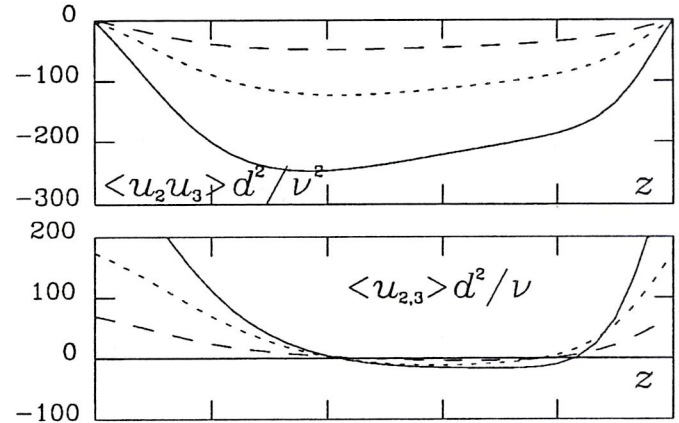


Fig. 2. The profiles of  $u_2 u_3$  and  $u_{2,3}$  (normalized with  $d^2/\nu^2$  and  $d^2/\nu$ , respectively). The solid lines are for  $U_{23} = 1.0$ . The dotted and dashed curves refer to runs with  $U_{23} = 0.5$  and  $0.2$ , respectively

#### 4.3. Turbulent heat conductivity

Let us finally consider the turbulent heat conductivity  $\chi_t$ . In a compressible stratified medium the convective flux  $\mathbf{F}_{\text{conv}} = \gamma \langle \epsilon \rho \mathbf{u} \rangle$  scales with the entropy gradient,  $\nabla \langle s \rangle$ , via

$$\mathbf{F}_{\text{conv}} = -\chi_t \langle \gamma \epsilon \rangle \langle \rho \rangle \nabla \langle s / c_p \rangle. \quad (14)$$

The resulting profile for  $\chi_t$  is displayed in the lower panel of Fig. 3. In the upper panel are also shown the  $z$ -components of  $\mathbf{F}_{\text{conv}}$  and  $\mathbf{F}_{\text{rad}}$ .

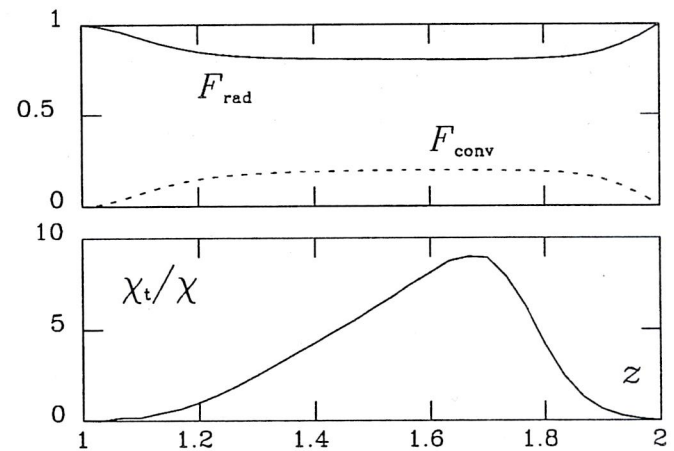


Fig. 3. The profiles for  $\chi_t$  normalized with  $\chi = \mathcal{K}/\rho_0$  (lower panel) and the  $z$ -components of  $\mathbf{F}_{\text{conv}}$  and  $\mathbf{F}_{\text{rad}}$  normalized with the total flux (upper panel)

## 5. The mean Lorentz force

The presence of a systematic mean current  $\langle \mathbf{J} \rangle$  in the simulations allows us to investigate also the mean Lorentz force  $\langle \mathbf{J} \times \mathbf{B} \rangle$ . This quantity has been investigated recently by Rüdiger & Kichatinov (1990). They have stressed that for a wide class of turbulence models it is possible for  $\langle \mathbf{J} \times \mathbf{B} \rangle$  to degenerate to a gradient term. This would have dramatic consequences for the theory of the solar torsional oscillations. Note however that this result is obtained in the framework of the first order smoothing approximation. The result for  $\langle B'_i B'_j \rangle$  derived by Rüdiger & Kichatinov is similar to that found by Roberts & Sowards (1975) and it leads to

$$\langle \mathbf{J} \times \mathbf{B} \rangle = -\left(\frac{\eta t}{\eta} - 1\right) \langle \mathbf{J} \rangle \times \langle \mathbf{B} \rangle - \frac{\eta t}{\eta} \nabla \langle \mathbf{B} \rangle^2 / \mu_0. \quad (15)$$

In Fig. 4 we present the result for  $\langle \mathbf{J} \times \mathbf{B} \rangle$  obtained from our simulations taking Eq. (11) as boundary condition. Additionally we take  $B_3 = B_0$  as initial condition. This leads to a constant  $\langle B_3 \rangle$ , following from  $\text{div} \langle \mathbf{B} \rangle = 0$  and the assumption of periodic boundary conditions in the horizontal direction (Paper I). The systematic Lorentz force is expected to be  $\langle \mathbf{J} \rangle \times \langle \mathbf{B} \rangle \approx (0, d, d - z) B_0^2 / \mu_0 d^2$ .

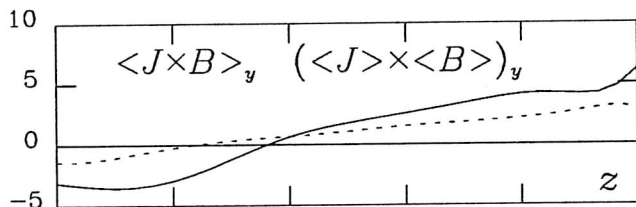


Fig. 4. The  $y$ -component of  $\langle \mathbf{J} \times \mathbf{B} \rangle$  (solid lines) compared with  $\langle \mathbf{J} \rangle \times \langle \mathbf{B} \rangle$  (dotted lines). The curves are in units of  $B_0^2 / \mu_0 d$

The result for the  $y$ -component of  $\langle \mathbf{J} \times \mathbf{B} \rangle$  is shown in Fig. 4. We see that  $\langle \mathbf{J} \times \mathbf{B} \rangle_y$  is twice as large as  $(\langle \mathbf{J} \rangle \times \langle \mathbf{B} \rangle)_y$ . This is in contrast to Eq. (15), which would predict the opposite behavior.

One should bear in mind that the results presented here cannot be compared directly with those obtained in the framework of first order smoothing. Both approaches represent two extreme cases: here we deal with relatively slow and smooth flows confined in a thin layer whereas first order smoothing is applicable only to flows with short correlation time and short correlation length. Our results should therefore merely be understood just as a demonstration of the other extreme.

## 6. Discussion

The present investigations have shown that convective turbulence can efficiently smooth advected quantities ( $\mathbf{B}$ ,  $\mathbf{u}$ , and  $s$ ) in the vertical direction. The approach to describe this by  $z$ -dependent diffusivities may be in some cases questionable. This becomes evident in particular when the vertical gradients of these quantities change sign. It is also questionable, whether the retained  $z$ -dependence of the averages is useful.

The correlation length in the  $z$ -direction is in our model already comparable with the height of the box. Alternatively one could therefore average also over the  $z$ -direction

This result that advected quantities are efficiently smoothed out in the vertical direction may have implications for understanding properties of the solar differential rotation. The dominant feature of convective motions are isolated, fast, filamentary, and twisting downdrafts that merge into successively larger scale downdrafts with depth (Stein & Nordlund, 1989). Such filamentary downdrafts may work to "stiffen" the vertical structure. Only near the boundaries does this mechanism become ineffective and deviations from radial rotation contours can occur.

As long as it is impossible to resolve sufficiently small scales in a global 3-D simulation it may be useful to incorporate a mean-field approach with simulations of the small-scale behavior. The ultimate aim would be to apply the results for the derived mean-field transport coefficients to the computation of such global models. However, there are major problems with this approach. The presence of artificial boundaries, the only slightly turbulent flow, and the relatively short range of different length scales are all unrealistic properties of our simulated flow. It might appear reasonable to identify the computational boundaries with the upper and lower boundaries of the convection zone. This would be, however, incompatible with the idea of examining the turbulent flow only in a small test volume. The present investigations have demonstrated that the test volume concept allows us to impose systematic gradients. This is important, because plausible results for the turbulent diffusivities were only obtained after imposing such gradients.

Future investigations should be performed also with quite different boundary conditions, because this can give some information about the restrictions imposed by such conditions. It has now become feasible to perform a number of runs with different magnetic field strength (Chandrasekhar number) to see at what parameter values nonlinear effects set in. Similarly a possible saturation for high inverse Rossby numbers might be detected by varying the ratio of Taylor number to Rayleigh number. Investigating the dependence of the  $\alpha$ -effect on latitude as well as on the field orientation would provide a further test.

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